

RESOLUTION NO. U-11199

A RESOLUTION authorizing adoption of the Washington State Department of Commerce Advisory Opinion WA2020-001 for renewable resources compliance for the Washington Energy Independence Act (I-937).

WHEREAS the City of Tacoma, Department of Public Utilities, Light
Division (d.b.a. "Tacoma Power") completed a rebuild in December of 2011, of
the turbines, transformers and wicket gate seals at Generators 51 and 52
located at the Mossyrock Dam Powerhouse, and

WHEREAS the Rebuild upgrades and the associated savings meet the requirements for a qualifying eligible renewal resources per RCW 19.285.040(2)(e) and WAC 194-37-130, and will assist in Tacoma Power's compliance with the Washington Energy Independence Act; and

WHEREAS a report updating and revising Tacoma Power's modeling to reflect actual stream flows for the most recent years and a request for an Advisory Opinion was submitted to the Washington Department of Commerce, per RCW 19.285.045 (2), on January 29, 2020, and

WHEREAS the Washington Department of Commerce advisory opinion process requires adequate information and a fee of \$1,250 to perform a legal analysis and provide for a public comment period, and

WHEREAS as the Department of Commerce received no public comments, and the Department of Commerce agreed with Tacoma Power's modeling and issued its Advisory Opinion WA2020-001, on April 29, 2020, and

WHEREAS the savings from adopting this Advisory Opinion are estimated to save Tacoma Power approximately 44,800+ MWh plus an



additional 20% credit for using qualifying apprenticeship labor, for an estimated annual total of 53,760 MWh, which will assist in meeting the renewal standards for the Washington Energy Independence Act without purchasing additional renewable resources such as third-party renewable energy credits (valued at \$2-\$6/MWh), with an estimate savings of \$107,520 to \$322,560, and

WHEREAS a public hearing was conducted by the Board on September 23, 2020, as required by RCW 19.285.045 (2), Now, Therefore,

BE IT RESOLVED BY THE PUBLIC UTILITY BOARD OF THE CITY OF TACOMA:

That the Department of Commerce Advisory Opinion, in the form as on file with the Clerk, is adopted.

Approved as to form:		
Approved do to form.	Chair	
/s/		
Chief Deputy City Attorney	Secretary	
	Adopted	
Clerk	• • • • • • • • • • • • • • • • • • • •	





TO:

Jackie Flowers, Director of Utilities

COPY:

Charleen Jacobs, Director and Board Offices

FROM:

Clay Norris, Section Manager - Power Management

MEETING DATE:

September 23, 2020

DATE:

September 2, 2020

SUMMARY:

Adopt by resolution and public hearing Washington State Department of Commerce Advisory Opinion WA2020-001 per RCW 19.285.045 (2) for renewable resources compliance with the Washington Energy Independence Act (also known as 1937) involving approved engineering modeling for incremental hydro savings due to the 2011 rebuild at Mossyrock Dam/Powerhouse.

Per the advice of the Washington State Auditor's Office from our successful 2018 renewable compliance audit with the Washington Energy Independence Act RCW 19.285, our previous modeling of the Mossyrock Rebuild was dated (2010) and needed to reflect actual stream flows for the most recent years.

BACKGROUND: Provide information that is required to orient the Board. Provide context and frame the issue or topic.

In December 2011, Power completed a rebuild of the turbines, transformers and wicket gate seals at Generators 51 and 52 located at the Mossyrock Dam Powerhouse. These Rebuild upgrades and the associated savings qualify as a qualifying eligible renewable resource per RCW 19.285.040 (2) (e) and WAC 194-37-130 to meet portions of annual renewable resource compliance with Washington Energy Independence Act. The renewable savings plus apprenticeship labor credited were based on 2010 engineering modeling. Per the advice of the State Auditor's Office needed to reflect actual stream flows for the most recent years. A team of Ahlmahz Negash, Power Analyst with Power Management, Tyler Braun with Generation along with John Walkowiak, Conservation Operations Manager saw the opportunity update and revise the modeling report and submitted an Advisory Opinion to the Washington Department of Commerce per RCW 19.285.045 (2) on January 29, 2020.

Commerce's advisory opinion process requires adequate documentation, fee of \$1,250 to perform a legal analysis and public comment period. There were no public comments regarding the Mossyrock Rebuild renewable energy savings. Commerce.agreed with Tacoma Power's modeling and issued Advisory Opinion WA2020-001 on April 29, 2020.

The savings from this Advisory Opinion are estimated to save Tacoma Power approximately 44,800+ MWh plus an additional 20% credit for using qualifying apprenticeship labor for an estimated annual total of 53,760 MWh to assist in meeting the renewable standards for the Washington Energy Independence Act without purchasing additional renewable resources such as third-party renewable energy credits (valued at \$2-\$6/MWh). Power Management estimates the annual cost savings to range from \$107,520 to \$322,560.





ARE THE EXPENDITURES AND REVENUES PLANNED AND BUDGETED? No.

IF THE EXPENSE IS NOT BUDGETED, PLEASE EXPLAIN HOW THEY ARE TO BE COVERED. Explain how expenditures are to be covered and if budget modifications are required.

IF THE ACTION REQUESTED IS APPROVAL OF A CONTRACT, INCLUDE LANGUAGE IN RESOLUTION AUTHORIZING \$200,000 INCREASE IN ADMINISTRATIVE AUTHORITY TO DIRECTOR? No.

ATTACHMENTS: Washington Department of Commerce - Energy Office Advisory Opinion WA2020-001

CONTACT:

John Walkowiak, Conservation Operations Manager (253) 316-6002 (cell) jwalkowiak@cityoftacoma.org and Ahlmahz Negash, Power Analyst anegash@cityoftacoma.org Provide supervisor's name. Ray Johnson, Assistant Power Section Manager II Provide name of presenter at podium if different from primary contact.



commerce.wa.gov/eia

Washington State
Energy Independence Act

Application for Advisory Opinion and Renewable Energy Facility (WREGIS) Certification

County: Lewis

Country: USA

A separate Washington application is required for FACILITY NAME: Mossyrock Hydroelectric Project each generating unit with a separate WREGIS GU WREGIS Generating Unit ID (if already registered): ID. Applicant must select Washington in WREGIS generating unit registration. Section 1: Agency Action Requested Advisory Opinion and WREGIS Certification Advisory Opinion Only Section 2: Applicant Information Applicant Contact: John Walkowiak Title: Cons Ops Manager Applicant Phone: (253) 502-8534 Applicant E-mail: jwalkowiak@cityoftacoma.org Applicant Company Name: Tacoma Power/Tacoma Public Utilities Company Address: 3628 South 35th Street City: Tacoma State/Province: WA Zip Code: **98409-3192** Country: USA **Section 3: Facility Information Facility Owner** Name of Facility Owner: OR The Facility Owner is the same as the Applicant.

All information provided in this application or any supplemental or additional materials is subject to public disclosure.

City: Mossyrock

Facility Name: Cowltiz River Project

Contact Name, Phone, and Email: Facility Identification and Location

Unit Name: Mossyrock Dam

Address:

City/State/ZIP:

State/Province: WA Zip: 98564

Unit location (street address, legal description, or GPS coordinates): WGS84 Coordinates 46 32'4"N, 122 25'43" W or 46.534444, -122.428611

Provide a description of the facility.

Mossyrock Dam completed by Tacoma Power in 1968 at a cost of \$117.8 million and is Washington state's tallest dam at 606 feet above bedrock (or 365 feet above the Cowlitz Riverbed. The dam's double curvature concrete arch has three penstocks between 248 and 285 feet in length that extend down to the Mossyrock Powerhouse that contains two turbine/generators (Unit 51 and Unit 52) with nameplate rating of 382,000 kW. The Mosyrock Dam created 23.5 mile long Riffe Lake. The Mossyrock Rebuild project replaced/upgraded the the two 150,000 kW turbine generators, Transformers and wicket gate sealing for both Units that were 40+ years-old in 2010 and 2011 at a cost of \$54 million.

	Application 2020-0	01	
Eacility Idou	ntification Numbers		
			Mh an Futair al IDi
EIA Utility C	nerating Unit ID: Pending		Other External ID: A Plant Code:
		CIF	A Flaint Code.
A. Facility P	Facility Eligibility		and the state of t
	Capacity (MW): 382		
	will change, please explain:		
	Operation Date (COD): 10 / 13 / 1968		
		Ma	
If yes, pleas	ity considered repowered by WREGIS? Yes	IVO	
B. Facility F	uel		
Indicate ead	ch energy source used by the facility. For definition	ns, refe	r to <u>RCW 19.285.030</u> . For multi-fuel generating
facilities inc	licate all fuels used.		
Wine	d		Wave power
Sola	r energy		Ocean power
	thermal energy	Ħ	Tidal power
	Ifill gas		Gas from sewage treatment facility
	nass energy (must complete Section 5)		Biodiesel fuel (must complete Section 6)
	er (must complete Section 7)	H	Other (please specify):
	ility use any fossil fuel or other non-qualifying fuel	? \\\ Y6	
	fossil fuel or other non-qualifying fuel:		
1	e annual amount of non-qualifying fuel used (perc	ent of r	net heat input):
Section 5:	Biomass Energy Supplement (complete only i	f "bior	nass energy" is checked in Section 4)
Allowed Fu	el Sources. Indicate each source of biomass energ	y used	by the facility.
Orga	nic by-products of pulping and the wood		Food waste and food processing residuals
- -	ufacturing process		Tool made and took processing residuals
	nal manure		Liquors derived from algae
Solid	l organic fuels from wood		Dedicated energy crops
Fore	st or field residues		Yard waste
Untr	eated wooden demolition or construction debris		
	Fuel Sources. The following materials will NOT be	used as	s a source of hiomass energy by the facility
	nd pieces that have been treated with chemical		Wood from old growth forests
	ervatives such as creosote, pentachlorophenol,		
l I	opper-chrome-arsenic		Municipal solid waste
	nass. The Washington Energy Independence Act a	llows a	biomass energy facility commencing operation
	ch 31, 1999 to qualify as an eligible renewable res		_ ,
	cation requirements.		

Sectio	n 6: Biodiesel Fuel Supplement (complete only if "biodiesel fuel" is checked in Section 4)
	odiesel fuel used by the facility meets each of the identified conditions:
	The fuel (a) is a mono alkyl ester of long chain fatty acids derived from vegetable oils or animal fats for use in compression-ignition engines and (b) meets the requirements of the American society of testing and materials specification D 6751 in effect as of January 1, 2003.
	The fuel is NOT from crops raised on land cleared from old growth or first-growth forests where the clearing occurred after December 7, 2006.
Sectio	n 7: Water/Hydroelectric Power (complete only if "water" is checked in Section 4)
The fa	cility uses water as a fuel in the following manner:
	Incremental Hydro. Incremental electricity produced as a result of efficiency improvements completed after March 31, 1999, to hydroelectric generation projects owned by a qualifying utility and located in the Pacific Northwest where the additional generation does not result in new water diversions or impoundments.
	Date efficiency improvement completed: 12/1/2011
	Method of measuring incremental generation:
	Incremental generation is separately metered or measured.
	Incremental generation is modeled each year based on actual stream flows.
	Incremental generation is modeled as a fixed percentage of total generation. Fixed percentage: %
	Incremental generation is modeled as a fixed generation amount. Fixed amount: megawatt-hours
	Note: If any box but the first is checked, the facility must register in WREGIS as a multi-fuel facility.
	Non-incremental generation will be classified as Large Hydro (LHN) and excluded from certificate creation.
	Canal or pipe. Hydroelectric generation from a project completed after March 31, 1999, where the
	generation facility is located in irrigation pipes, irrigation canals, water pipes whose primary purpose is for
	conveyance of water for municipal use, and wastewater pipes located in Washington where the generation
	does not result in new water diversions or impoundments.
Sectio	n 8: Eligibility for Washington Multipliers (Optional)
The fac	cility qualifies for the following multipliers under the Washington Energy Independence Act:
	Distributed Generation. The facility has a generating capacity of 5 MW or less and is not part of any
	integrated cluster of facilities with an aggregate generating capacity of 5 MW or more.
	Apprentice Labor. The facility commenced operation after December 31, 2005 and in construction used an apprenticeship program approved by the Washington State Apprenticeship and Training Council.
I	Commerce requests optional multiplier eligibility from facility owners for informational purposes only. Owners seeking ation of a facility as eligible for a multiplier should contact Commerce for application requirements.
Sectio	n 9: Reservation
Energy that inf certific	ashington Department of Commerce makes a determination of resource eligibility under the Washington Independence Act based on the information provided by the applicant and does not independently verify formation. An applicant must promptly notify Commerce of any changes to the information submitted for ation that may affect the facility's eligibility. Commerce reserves the right to modify or withdraw a action if it determines that the information supplied by the applicant was incomplete or inaccurate.

Section 10: Attestation

I declare that the information provided in this application and any supplemental forms and attachments are true and correct to the best of my knowledge, that the information contained in this submission is consistent with information on file with WREGIS unless otherwise indicated, that no information materially affecting the facility's eligibility has been withheld, and that I am authorized to file this submission on the facility owner's behalf.

Signature: Kyr

Date Signed: 1/29/2020

Authorized Officer/Agent: Ray Johnson

Officer Title and Company: Power Section Assistant Manager II

Name of Facility: Tacoma Power - Mossyrock Dam

Application Checklist for Submission

Applicants must select the Washington program administrator in the generating unit's WREGIS static data. Applicants should ensure that the following documents are provided:

- 1. Electronic copy of entire application, including a signed attestation page.
- 2. WREGIS "static data" if the facility is already registered in WREGIS. A printout of your generator account profile screen in WREGIS.
- 3. Optional project background documentation. Background documentation can be submitted or published in regulatory settings (FERC or state commission filings) or informal forums (websites, articles or factsheets).
- 4. Payment of advisory opinion fee of \$1,250. A separate application and application fee are required for each generating unit. However, if a facility owner has multiple WREGIS generating unit IDs for a single facility and all the static characteristics of the facility (other than the generating capacity) are identical, it may request that Commerce treat the combined generating units as a single application. The owner must document at the time of application that all GU IDs are part of a single facility in a single location. If GU IDs are added later, a separate application will be required.

To submit your facility for certification, e-mail the application and any supplemental materials listed above to (wregis@commerce.wa.gov). Submit payment of the advisory opinion fee to:

Department of Commerce Attn: State Energy Office

P.O. Box 42525

Olympia, WA 98504-2525

Commerce will post each application on its website. Applications are subject to a public comment period.

	Advisory Opinion and WREGIS Certification (to be completed by Commerce)												
It is t	It is the opinion of the Washington Department of Commerce that the facility identified in this application meets the												
	statutory legal standard for an eligible renewable resource as defined in RCW 19.285.030, based on the factors set												
out b	out below The facility will be designated in WREGIS as an eligible renewable resource under the Washington Energy												
Inde	ndependence Act:												
Facili	Facility Name: Mossyrock Hydroelectric Project WREGIS GU ID:												
X	The fuel source for the facility is identified in RCW 19.285.030 as renewable energy:												
		Win	d			Wave, ocean, or	r tidal power						
	☐ Solar energy ☐ Gas from sewage treatment facilities												
	☐ Geothermal energy ☐ Biodiesel fuel												
		Lan	dfill gas			Biomass energy							
	x	Wat	er (incremental efficiency hyd	dro)		Water (pipe or o	canal)						
х	The	facili	ty commenced operation afte	er March 31, 199	99, as	required by RCW	19.285.030.						
	The	facili	ty is located in the Pacific Nor	thwest, or the e	lectri	city from the faci	lity is delivered into						
X	Was	shing	ton state on a real-time basis	without shaping	g, stor	age, or integratio	on services, as required						
	by F	RCW :	19.285.030.										
Addi	tiona	al Pro	Incremental generat visions:flows and using the part of the applicatio	method provide			ased on actual water analysis provided as						
Was	hingt	on Ce	ertification Number: WA	\2020-001									
				WAS	HING	TON DEPARTME	NT OF COMMERCE						
				Mich	nael F	Furze, by email	2020-04-29						
				Direc	tor o	r Designee	Date						

Renewable Incremental Hydro Mossyrock Rebuild

Mossyrock Dam Tacoma Power/Tacoma Public Utilities

New Turbines, Transformers and Wicket Gate Sealing Advisory Opinion Application/Documentation



January 30, 2020



Renewable Incremental Hydro Report

Mossyrock Rebuild

TABLE OF CONTENTS

Overview/Summary	3
Washington RPS Eligibility	3
Project Location and Site Description	4
Engineering Review – Turbine Rebuild	5
Engineering Review – Transformer Replacement	15
Engineering Review – Wicket Gate Sealing	21
Summary	24

Overview/Summary

Tacoma Power, dba Light Division of Tacoma Public Utilities, is seeking Advisory Opinion approval of its engineering calculations/modeling for the incremental hydroelectric energy gains from the rebuild of our Unit 51 (2010) and Unit 52 (2011) turbines, generators and wicket gates sealing located at our Mossyrock Hydroelectric Project (Mossyrock) in Lewis County, WA. We believe that the incremental energy gains per year are eligible for Washington state's Renewable Portfolio Standard (RPS) per RCW 19.285.030 (12) (b). Tacoma Power proposes that Units 51 and 52 will be registered in the Western Renewable Energy Generation Information System (WREGIS) as a group and the incremental energy savings will be annually updated and reported as part of a proposed Qualified Reporting Entity (QRE) agreement and logged with WREGIS. The following report summarizes the engineering calculations/modeling developed and Tacoma Power's determination of incremental hydroelectric savings. Table 1 below summarizes our findings using actual 2018 Generation data.

Table 1: Mossyrock Rebuild Incremental Hydro - Summary Using 2018 Generation Data

Rebuild Action	Incremental Hydro Savings (MWh)
Turbine Rebuild	24,534
Transformer	1,200
Replacement	
Wicket Gate Sealing	19,099
Totals	44,833

Washington RPS Eligibility

Incremental hydroelectric energy savings are qualified under RCW 19.285.030 (12)(b), which allows incremental electricity produced as a result of efficiency improvements completed after March 31, 1999 to qualify as an eligible renewable resource. Tacoma Power is submitting this Advisory Opinion report to register the incremental hydroelectric efficiency gains in WREGIS accordance with WAC 194-37-130 (3) (c) (ii) Method One – actual incremental generation.

Project Owner

Project Owner	Tacoma Power – dba Light Division Tacoma Public Utilities
Street Address	3628 South 35 th Street, Tacoma WA 98409-3192
Mailing Address	P.O. Box 11007, Tacoma, WA 98411-0007
Project Representatives	John Walkowiak, Conservation Operations Manager
	Ahlmahz Negash, Power Analyst
	Tyler Braun, PE, Power Engineer III
Phone	(253) 502-8534; (253) 502-8093; (253) 502-8658
Email	jwalkowiak@cityoftacoma.org;
	anegash@cityoftacoma.org:
	tbraun@cityoftacoma.org
Fax	(253) 502-8572
Website	www.mytpu.org

Project Location and Site Description

The Mossyrock Dam and Hydroelectric facility is part of Tacoma Power's Cowlitz River Project located in eastern Lewis County, WA. Mossyrock Dam was completed by Tacoma Power in 1968 at a cost of \$117.8 million and is Washington State's tallest dam at 606 feet above bedrock (or 365 feet above the Cowlitz Riverbed). The dam created 23.5-mile-long Riffe Lake. The dam's double-curvature concrete arch has three penstocks between 248 and 285 feet in length that extend down to the powerhouse. The powerhouse contains two turbine generators (Unit 51 and Unit 52) with a combined nameplate rating of 382,000 kW.



Figure 1: Location of the Mossyrock Dam and Hydroelectric Project

The \$50 million Mossyrock Rebuild project began in March 2008, replacing and/or upgrading the original, 40-year-old turbines, generators, exciters, plant controls, transformers and wicket gate end seals for Units 51 (completed 2010) and Unit 52 (completed in 2011) and increasing total capacity by 70 MW with peak overall energy conversion efficiency near 95%.



Figure 2: Mossyrock Dam Photo, October 2019

Engineering Review

Mossyrock Rebuild Turbine Calculations/Modeling

Because it is not possible to directly measure the incremental hydro generation from our Mossyrock turbine rebuild project, Tacoma Power originally utilized a Vista LT hydro optimization model (Vista) for RPS reporting years 2010-2014. The Vista model utilized historical inflows for an 75-year period from 1929-2003, Tacoma Power developed "Content Tables" for reservoir water elevations for the range of turbine operations within 621-780 ft. and a set of I/O curves that reflected unit characteristics before (pre-) and after (post-) rebuild. Starting in 2016, Tacoma Power updated the historical Riffe Lake inflows for the period 2004 through 2018 (Figure 3) in order to meet compliance requirements that the most readily available stream flow records be used to provide annual incremental hydro savings per WAC 194-37-130 3 (c) (ii) or (iii).

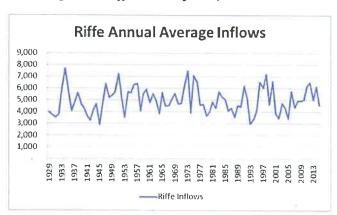


Figure 3: Riffe Lake Inflows, 1929-2018

Tacoma Power no longer utilizes the Vista model. Since the amount of efficiency improvement will vary from year to year because of changing reservoir inflows and operating conditions, we plan to provide actual annual generation savings utilizing Method One of WAC 194-37-130 (3) (c) (i), using the following engineering model (Equation 1) of hydropower generation, P, as a function of turbine efficiency, η_t , generator efficiency, η_g , flow through the turbine, Q, and net head, h_{net} , to calculate pre- and post-rebuild turbine efficiency. To show validity of Equation 1, we used it to calculate an average percentage incremental generation over a historic period and assumed similar operating conditions both before (pre-) and after (post-) rebuild.

$$P = \eta_t \eta_g \left(\frac{1000 kg}{m^3}\right) \left(\frac{9.81 m}{s^2}\right) \frac{h_{net}}{\frac{3.28 ft}{m}} \frac{Q}{\left(\frac{3.28 ft}{m}\right)^3} \left(\frac{10^{-6} MW}{W}\right) \quad \text{(Equation 1)}$$

Historic Calculation Period:

The historic calculation period spanned 2011 – 2018. These years represent a range of wet, dry and average water conditions as well as a significant change in operations for the Mossyrock project. Starting in 2016, the United States Geological Survey (USGS) revised its earthquake predictions for the Cowlitz River Basin. To protect public safety, Tacoma Power began holding Mossyrock's Riffe Lake

maximum elevation approximately 30 feet below full. This lower lake elevation is likely to remain in effect at least into the next decade. The new lower maximum lake elevation is of particular significance given that the efficiency upgrade for Mossyrock's Unit 51 was designed to reach maximum turbine efficiency at lower lake elevation.

Data Requirements:

The data required for this analysis involved:

- Post-Rebuild Generation and Elevation were acquired actual hourly measurements of generation and lake elevation for each Mossyrock Project unit (Unit 51 and Unit 52) during the post-rebuild historic period
- 2. Post-Rebuild Turbine Efficiency Tables were created using field test measurements of each unit's turbine efficiency after the rebuild, at various lake levels and various levels of flow through the turbines.
- 3. Pre-Rebuild Turbine Efficiency Tables were created using field test measurements of each unit's turbine efficiency prior to the rebuild, at various lake levels and various levels of flow through the turbines.

Analysis - Amount of Incremental Generation

Using Equation 1, field test measurements of unit efficiency were used to create lookup tables for post-rebuild (Table 2) and pre-rebuild (Table 3) flow, generation, and elevation sets. Given any feasible set of generation and lake level, the corresponding flows through the unit can be determined in the look-up tables; alternatively, given a set of flow and elevation, the corresponding powers could be determined in the post-rebuild lookup table. It is worth noting here that the efficiency upgrade changed the feasible operating range of the turbines (in terms of elevation and flow), as illustrated in Figures 4 and 5.

The following describes the 6-step methodology used to calculate the amount of incremental hydro generation of the Mossyrock upgrade using the data described above:

1. Created "Post-Rebuild Turbine Efficiency Tables" (Table 2) for New Units 51 and 52 using new efficiency curves (Figures 4 & 5) based on field testing conducted post-rebuild (table row = power output in MW, table column = lake elevation in ft).

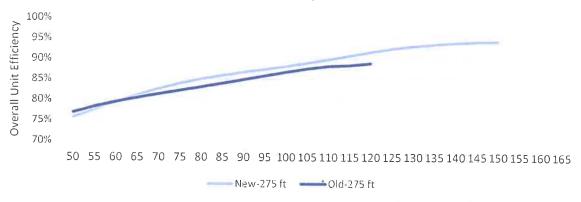
	700	705	710	715	720	725	730	735	740	745	750	755	760	765	770	775	778.5
0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5	1061	1056	1055	1054	1055	1057	1060	1059	1049	1029	1005	977	952	925	892	854	827
10	1354	1328	1311	1296	1286	1274	1263	1250	1231	1207	1183	1164	1144	1124	1103	1084	1067
15	1553	1521	1488	1461	1444	1429	1411	1393	1368	1341	1320	1300	1282	1272	1263	1245	1226
20	1726	1689	1652	1617	1592	1572	1552	1528	1500	1473	1449	1432	1419	1415	1406	1386	1370
25	1897	1851	1815	1783	1751	1724	1700	1670	1639	1612	1589	1579	1572	1562	1545	1526	1512
30	2077	2020	1982	1955	1928	1900	1871	1838	1805	1779	1761	1749	1734	1712	1 691	1676	1664
35	2270	2206	2161	2134	2117	2103	2081	2049	2018	1992	1968	1937	1908	1878	1855	1832	1817
40	2479	2409	2364	2336	2317	2299	2276	2250	2223	2197	2171	2143	2111	2072	2031	2001	1985

Table 2: Step 1 – Post-Rebuild Flow Lookup Table (Flow, "cfs")

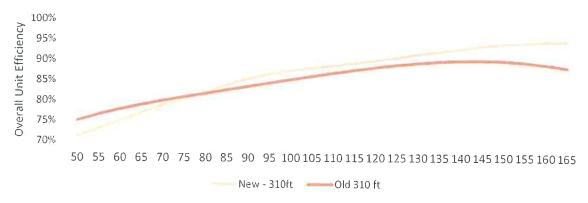
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45	2711	2628	2574	2538	2511	2495	2491	2464	2435	2404	2368	2333	2296	2259	2221	2184	2162
50	2935	2839	2773	2732	2708	2694	2697	2682	2653	2618	2571	2526	2480	2437	2397	2361	2341
55	3145	3047	2983	2933	2903	2888	2884	2871	2843	2809	2766	2717	2668	2618	2571	2529	2507
60	3356	3256	3184	3131	3090	3070	3061	3046	3019	2990	2947	2898	2845	2792	2740	2696	2672
65	3550	3454	3382	3326	3282	3253	3234	3215	3190	3160	3120	3071	3017	2962	2913	2865	2838
70	3747	3654	3584	3529	3482	3444	3410	3382	3358	3334	3298	3248	3195	3139	3083	3033	3005
75	3949	3857	3790	3734	3685	3639	3596	3557	3526	3506	3473	3424	3370	3312	3257	3208	31 79
80	4156	4072	4000	3940	3888	3837	3785	3737	3696	3664	3635	3596	3546	3486	3428	3377	3349
85	4363	4285	4218	4154	4094	4035	3976	3918	3863	3820	3786	3747	3702	3652	3602	3551	3518
90	4577	4504	4436	4369	4302	4236	4169	4099	4033	3980	3938	3899	3859	3814	3766	3717	3681
95	4795	4725	4659	4592	4516	4440	4361	4283	4211	4152	4102	4058	4015	3973	3928	3877	3841
100	5016	4947	4876	4801	4725	4645	4558	4474	4399	4335	4280	4232	4185	4137	4088	4037	4000
105	5238	5163	5090	5014	4931	4846	4759	4675	4599	4531	4468	4409	4355	4305	4256	4203	4165
110	5462	5378	5297	5213	5127	5041	4956	4872	4795	4723	4655	4592	4534	4480	4427	4373	4335
115	5686	5593	5500	5408	5318	5233	5150	5068	4989	4917	4848	4779	4716	4657	4601	4544	4504
120	5907	5803	5701	5602	5511	5425	5340	5257	5178	5106	5037	4970	4905	4839	4778	4718	4675
125	6131	6016	5904	5802	5707	5618	5531	5445	5364	5290	5220	5152	5086	5022	4957	4892	4845
130	6361	6236	6120	6011	5909	5811	5720	5630	5545	5468	5398	5330	5264	5199	5132	5063	5014
135	6603	6472	6348	6228	6116	6012	5913	5818	5730	5649	5576	5507	5440	5373	5303	5232	51 79
140	6863	6719	6584	6457	6337	6223	6114	6011	5916	5831	5755	5684	5614	5547	5476	5400	5344
145	7136	6980	6834	6696	6565	6441	6322	6208	6105	6014	5935	5861	5791	5721	5646	5567	5508
150		7256	7096	6946	6805	6669	6539	6417	6307	6208	6122	6043	5969	5892	5815	5733	5673
155				7212	7057	6909	6769	6638	6519	6410	6316	6229	6147	6067	5987	5901	5838
160					7323	7162	7011	6869	6740	6623	6519	6423	6334	6249	6162	6073	6007
165						7430	7265	7111	6972	6847	6732	6627	6529	6436	6344	6251	6185
170	.6						7532	7367	7218	7083	6957	6841	6732	6630	6532	6435	6365
175								7637	7477	7330	7192	7064	6945	6833	6726	6623	6551
180									7749	7588	7438	7298	7168	7045	6929	6819	6742
185										7860	7696	7544	7401	7268	7142	7022	6941
190												7802	7647	7502	7365	7236	7148
195													7906	7748	7599	7459	7365
200														8007	7846	7694	7592
205																7941	7831
210																	8083

Efficiency Curves Pre and Post Rebuild (based on actual field tests) Figure 4: Unit 51 Efficiency Curve Comparison





Unit 51 Efficiency Comparison at 310 ft



Unit 51 Efficiency Comparison at 345 ft

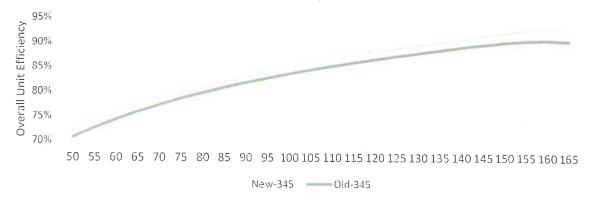
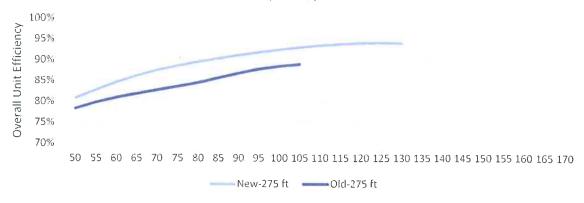
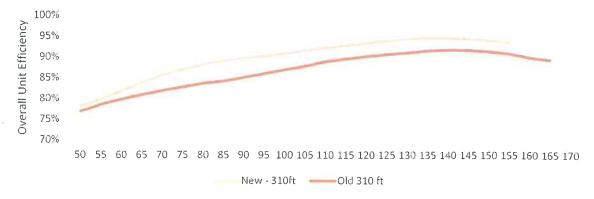


Figure 5: Unit 52 Efficiency Curve Comparison

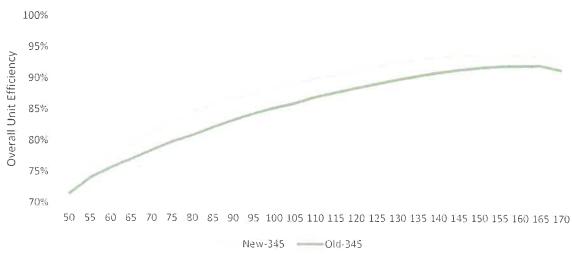
Unit 52 Efficiency Comparison at 275 ft



Unit 52 Efficiency Comparison at 310 ft



Efficiency comparison at 345 ft



2. Created "Pre-Rebuild Turbine Efficiency Tables" (Table 3) for old Units 51 and 52 using old efficiency curves (Figures 4 & 5) based on field testing just prior to rebuild (table row = flow in cfs, table column = lake elevation in ft.).

Table 3: Step 2 – Pre-Rebuild Power Lookup Table (Power, "MW")

	695	700	705	710	715	720	725	730	735	740	745	750	755	760	765	770	775	780
0					-											-		
250									Si									
500	(0)																	
750																		
1000									œ								,	
1250		11	12	12	12	13	13	13	13	13	13	14	14	15	15	15	16	
1500		18	18	19	19	20	20	20	21	21	21	22	22	22	22	23	23	
1750		23	25	25	26	27	27	28	28	28	29	29	29	30	30	30	30	
2000		27	31	32	32	33	33	33	34	35	35	36	36	37	37	37	38	
2250		30	33	37	39	40	40	41	41	42	43	43	43	44	44	44	45	
2500		42	43	44	45	45	46	47	48	48	49	50	50	51	51	52	52	
2750		47	48	49	50	51	52	53	54	55	56	56	57	57	58	59	59	
3000		53	54	55	56	57	58	59	60	61	62	63	63	64	65	66	67	
3250		58	59	61	62	63	64	65	66	67	68	69	70	71	. 72	73	74	
3500		63	65	.66	67	69	70 .	71	72	73	74	76	77	78	79	80	81	
3750		69	70	72	73	74	76	77	78	80	81	82	84	85	86	87	89	
4000		74	76	77	79	80	82	83	85	86	88	89	90	92	93	95	96	
4250		80	81	83	85	86	88	90	91	93	94	96	97	99	101	102	104	
4500		86	87	89	. 91	93	95	96	. 98	100	101	103	105	106	108	110	111	
4750		92	94	96	97	99	101	103	105	107	108	110	112	114	115	117	119	
5000		98	100	102	104	106	108	110	112	114	116	117	119	121	123	125	127	
5250		104	106	108	110	112	114	116	118	121	123	125	127	129	131	132	134	
5500		110	112	114	116	118	120	123	125	1,27	129	131	133	135	138	140	142	
5750		115	117	119	121	123	126	128	131	133	136	138	141	143	145	147	150	
6000			121	124	127	129	132	135	137	140	142	145	147	150	152	155	15.7	
6250					132	135	138	141	143	146	148	151	153	156	158	161	163	
6500							143	146	149	151	154	156	159	162	164			
6750								150	153	156	159	162	164					
7000										161	164						Ή	
7250																		
7500													2.0					2.7
7750																		
8000																		
8250						-		48										
8500																		

3. Collected actual Post-Rebuild Generation and Elevation data (Table 4) for years 2011-2018.

Table 4: Step 3 – Sample Post-Rebuild Generation and Elevation Data

YEAR	MONTH	DAY	HOUR	ELEVATION (FT)	POWER - U51 (MWH)	POWER - U52 (MWH)
2011	1	1	0	737	9	0
2011	1	1	₂₁ 1	737	0	0
2011	1	1	2	737	0	0
2011	1	1	3	737	0	0
2011	1	1	4	737	0	28
2011	1	1	5	737	0	109
2011	1	1	6	737	0	110
2011	1	1	7	737	52	112
2011	1	1	8	737	98	101
2011	1	1	9	737	100	93
2011	1	1	10	737	100	89
2011	1	1	11	737	77	98
2011	1	1	12	737	0	104
2011	1	1	13	737	0	89
2011	1	1	14	737	0	102
2011	1	1	15	737	0	101
2011	1	1	16	737	101	91
2011	1	1	17	737	111	90
2011	1	1	18	737	135	90
2011	1	1	19	737	151	90
2011	1	1	20	737	160	90
2011	1	1	21	737	153	90
2011	1	1	22	736	117	48
2011	1	1	23	736	120	0

- 4. Determined hourly post-rebuild flow (Table 5) through each unit: for each set of hourly, post-rebuild power and elevation data points, look up the corresponding flow in the "Post-Rebuild Flow Table". Exceptions:
 - i. If post-rebuild power is 0, then set flow to 0.
 - ii. If post-rebuild power is outside the feasible range of power in the "Post-Rebuild Flow Table", then set power to zero AND set flow to 0.
 - iii. If post-rebuild elevation is outside the feasible range of elevation in the "New Flow Table", then set power to 0 AND set flow to 0.
- 5. Determined pre-rebuild power for Units 51 and 52: With flow and elevation sets from Step 4, find corresponding pre-rebuild power using the "Pre-Rebuild Power Table" (Table 5). Exceptions:
 - i. If flow is 0, then set pre-rebuild power to 0.
 - ii. If flow is outside the range of the flows in the "Pre-Rebuild Power Table", then set pre-rebuild power to 0.

- iii. If elevation is outside the range of the elevations in the "Pre-Rebuild Power Table", then set pre-rebuild power to 0.
- 6. For each year, calculated average annual percentage of incremental hydro as the difference in post-rebuild power and pre-rebuild power divided by pre-rebuild power.

Table 5: Steps 4-6 – Post-Rebuild and Pre-Rebuild Power, Elevation, and Flow Delta Calculations for Sample 24-Hour Period

Step 4: Given			Step 5: Given Flo	w, look up Pov	Step 6: Calculate Difference					
Elevation, loo	k up									
Flow-U51		Flow-U52	Power-U51	Power-U52		Delta-U51	Delta-U52			
11	45	0	13.1		0	-4.1	0			
-	0	0	0.0		0	0.0	0			
	0	0	0.0		0	0.0	0			
	0	0	0.0		0	0.0	0			
	0	1595	0.0	24.9	405	0.0	3.0595			
	0	4529.5	0.0	103.0	615	0.0	5.9385			
	0	4720.5	0.0	103.0	615	0.0	6.9385			
276	2.5	4720.5	57.4	103.0	615	-5.4	8.9385			
43	41	4342	95.4	96.2	925	2.6	4.7075			
453	5.5	3952	102.3	82.9	045	-2.3	10.0955			
453	5.5	3749.5	102.3	76.6	205	-2.3	12.3795			
362	5.5	4152	75.9	89.4	775	1.1	8.5225			
	0	4342	0.0	96.2	925	0.0	7.7075			
	0	3749.5	0.0	76.6	205	0.0	12.3795			
•	0	4342	0.0	96.2	925	0.0	5.7075			
2.5	0	4342	0.0	96.2	925	0.0	4.7075			
453	5.5	1 3952	102.3	82.9	045	-1.3	8.0955			
493	0.5	3952	109.2	82.9	045	1.8	7.0955			
58	67	3952	135.3	° 82.9	045	-0.3	7.0955			
64	68	3952	147.2	82.9	045	3.8	7.0955			
692	0.5	3952	157.0	82.9	045	3.0	7.0955			
64	68	3952	147.2	82.9	045	5.8	7.0955			
51	23	2318.5	116.1	45.	355	0.9	2.645			
531	0.5	0	122.6		0	-2,6	. 0			

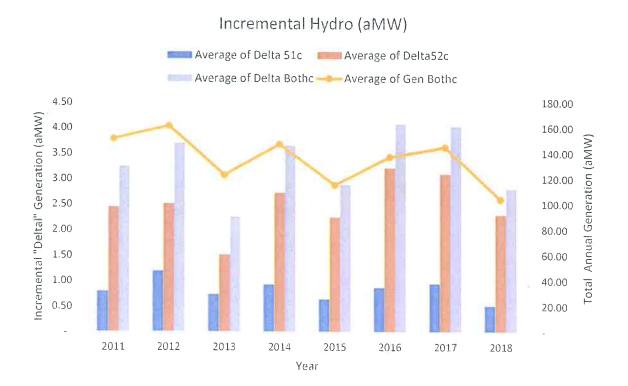
Table 6 and Figure 6 below summarize the average annual energy gains for the Mossyrock Turbine Rebuild for water years 2011-2018.

Beginning on January 1, 2020, Tacoma Power plans to calculate actual annual incremental energy gain (MWh) for the Mossyrock Turbine Rebuild for Washington RPS Method One compliance using Equation 1 and the associated tables and figures described for future RPS compliance periods.

Table 6: Calculated Average Annual Percentage/Savings of Incremental Hydro for Mossyrock Turbine Rebuild Units 51 & 52 Cambined, 2011-2018

	Incremental Generation (%)	Incremental Generation (aMW)	Incremental Generation (MWH)	
2011	2.14%	3.24	28,389	
2012	2.29%	3.70	32,391	
2013	1.83%	2.25	19,690	
2014	2.48%	3.65	31,973	
2015	2.50%	2.88	25,239	
2016	2.97%	4.08	35,703	
2017	2.79%	4.03	35,305	
2018	2.70%	2.80	24,534	
AVERAGE:	2.46%	3.33	29,153	

Figure 6: Results - Annual Incremental Hydro vs. Annual Generation



Engineering Review:

Mossyrock Rebuild Transformers Calculations/Modeling

During the Mossyrock Turbine Rebuild for Unit 51 (2010) and Unit 52 (2011), Tacoma Power replaced each of the two original (1967-68), Allis-Chalmers generator step-up (GSU) transformers with a bank of three one-phase transformers rated at 225 MVA in total.

We calculated the incremental hydro generation due to the transformer replacement based on the annual difference in losses of the new transformer banks and old transformer banks. This calculation required transformer performance testing of no-load and load losses (Table 7) as well as actual Unit 51 and Unit 52 generation data from 2011-2018. For each transformer bank (and for each year of generation data), we performed the following calculation:

1. Determined the "Loss Difference Vector", the difference between old and new transformer losses as a function of discrete transformer loading levels using measured no-load loss and loss at rated MVA (see Equation 2 and Table 7).

Table 7: Measured "No-Load Losses" and "Losses at Rated MVA" per Transformer (Three Transformers for Each of the Two Generating Units)

9		Rated Power (MVA)	No Load Loss (kW)	Losses @ Rated MVA (kW)
51	Old Transformer	54.7	45.4	216.3
5	New Transformer	75.0	47.5	206.7
52	Old Transformer	54.7	46.0	213.2
	New Transformer	75.0	47.3	205.5

Loss Difference
$$Vector_{MVA} = Loss_{No\ Load} + Loss_{rated\ MVA} \left(\frac{MVA}{rated\ MVA}\right)^2$$
 (Equation 2)

Figure 7: Unit 51 Loss Difference Vector

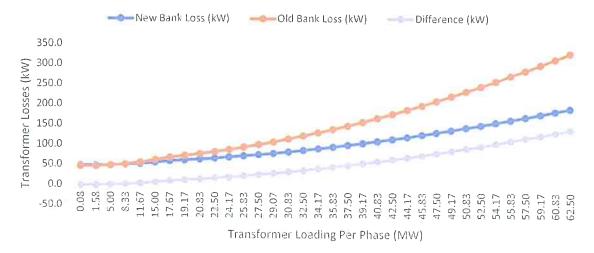


Figure 7: Transformer Losses as a Function of Transformer Londing Level (per Phase)

2. Determine the "Annual Operation Vector", the annual histogram of actual hourly generation data to determine the number of hours of operation in the aforementioned discrete transformer loading levels.

5000 4500 4000 3500 3000 2500 2000 1500 1000 500 0 0.08 1.58 5.00 8.33 11.67 15.00 17.67 19.17 22.50 24.17 25.83 27.50 29.07 30.83 34.17 35.83 34.17 35.83 34.17 Transformer Loading, Per Phase (MW)

Figure 8: Unit 51 Operation Summary (2018)

Figure 8: Generation Operation Summary for Unit 51 (for Year 2018)

3. Determine the annual incremental generation, the dot product of "Annual Operation Vector" and "Loss Difference Vector" multiplied by three to get the annual incremental hydro RECs for the three transformer phases.

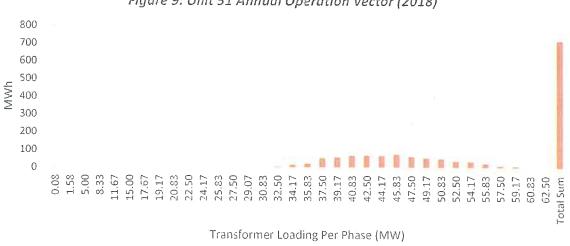


Figure 9: Unit 51 Annual Operation Vector (2018)

Figure 9. Histogram (Annual Operation Vector) for Unit 51 (for Year 2018)

¹ The dot product is the sum of the products of two vectors ("sum product" formula in MS Excel).

Tables 8 through 11 below summarize the data used for calculating incremental hydro generation for Units 51 & 52. Figures 7 through 9 above illustrate this calculation for Unit 51 and for the year 2018.

Table 8: Operations Summary for Unit 51, 2011-2018

Generation	2018	2017	2016	2015	2014	2013	2012	2011
MW	Hrs	Hrs	Hrs	Hrs		Hrs		Hrs
05	4513	3030	3429	4535	3186	2891	2537	4166
0-10	286	291	216	286	291	498	342	302
10-20	67	55	37	72	. 88	94	98	125
20-30	15	12	4	11	11	14	13	25
30-40	9	6	7	6	3	2		9
40-50	136	5	3	6	5			6
51-55	28	1	0	Ĩ.	0	1	3	4
56-60	9	1	1	3	0	2	2	
60-65	7	3	1			2		3
66-70	11	1	6	3	0		4	8
71-75	8	0		19	0		1	
76-80	11	2	4	26	3	3	1	3
81-85	3	2 6	- 1	24	6		11	3 6
86-90	11	11	14	23	4	36	10	10
91-95	24	14	13	13	39	105		13
96-100	47	30	12	41	80	158	78	72
101-105	129	231	242	136	163	247	135	127
106-110	180	. 284	302	182	223	281		126
111-115	376	373	366	168	259	325	265	160
116-120	380	405	457	229	278	399		
121-125	399	448	468	243	341	403		200
126-130	367	488	513	255	400	379		214
131-135	338	512	500	240	337	386		265
136-140	340	493	467	262	374	376	455	301
141-145	267	425	412	243	353	348	463	327
146-150	219	385	373	239	375	325		292
151-155	186	313	255	223	291	316	401	303
156-160	134	304	188	222	298	. 232	403	304
161-165	117	255	172	199	287	238	442	264
166-170	73	147	151	168	209	169		218
171-175	33	108	68	120	194	157	212	205
176-180	26	88	46	83	199	97	Appear to the state of the Party of the last	120
181-185	9	28	34	47	160	97	114	93
186-200	1	4	17	420	276	144	149	324
200-210	0	0	0	4	26	. 8		
210-220	0	0	0	0	0	0	0	C
	8759	8759	8783	8759	8759	8759	8783	8759

Table 9: Unit 51 Transformer Improvement

Mossyrock		Losses		Old Transformer	Tests (per	phase):	U51		New Trans	fonner Tests	(per phase)	: U51
Value Calcu	ulation											
			New Bank		Rated Pov				75.00	Rated Pow	er (MVA)	
			Old Bank	45.40	No Load L	oss (kW)		47.00	No Load Lo	ss (kW)	
				216.26	Load Loss	es @ Ra	ted MVA (kW))	206.60	Load Losse	s @ Rated i	VVA (kW)
		Each Phase	Each (1 of 3)	Each (1 of 3)			11-1				- j - m - j - m	†
Generation	Load	Xfmr Load	New Bank Loss	Old Bank Loss		Three						
MW	Avg		New Bank Loss	Old Bank Loss	Difference	Xfmrs						-
05	0.25	0.08	47.0	45.4	-1.6	-4.799					†	
.5-10	4.75	1.58	47.1	45.6	-1.5	-4.533					1	dis enablished
10-20	15	5.00	47.9	47.2	-0.7	-2.134			100000			
20-30	25	8.33	49.6	50.4	0.9	2.6061						ł
30-40	35	11.67	52.0	55.2		9.7159				A SERVICE MALERALIA		1
40-50	45	15.00	55.3	61.7		19.196					des en en en en	-
51-55	53	17.67	58.5	68.0		28,486						-
55-60	57.5	19.17	60.5	72.0	11.5	34.378		print a printer a c			1	
60-65	62.5	20.83	62,9	76.8		41,488				1		
65-70	67.5	22.50	65.6	82.0		49.19			= 255			
70-75	72.5	24.17		WITH SECURITION AND ADDRESS OF THE PERSON ADDRESS OF THE PER		57.485		** . ***********			+	1
75-80	77.5	25.83				66.372	rema					
80-85	82.5	27,50		100.1		75,852					÷	ļ
85-90	87.2	29.07	78.0	106.5		85,303						
90-95	92.5	30.83	The second secon			96.589						ļ
95-100	97.5	32,50				107.85				-	 	
100-105	102.5	34.17	89.9		39.9						·	
105-110	107.5	35.83			CONTRACTOR OF THE PARTY OF THE	132.14						
110-115	112.5	37.50			48.4					·	ł	
115-120	117.5	39.17			52.9	,					+	
120-125	122.5	40.83				173.02						
125-130	127.5	42.50		176.0		187.83						1
130-135	132.5	44,17				203.24						
135-140	137.5	45.83				219.23					·	÷
140-145	142.5	47.50	129.9			235.82				 		
145-150	147.5	49.17	135.8			253.01						ļ
150-155	152.5	50.83	141.9	71 10 77 7 7 7 7 7		270.78		U. E. 22		· · · · · ·		d
155-160	157.5	52.50				289.15		-			i	ļ
160-165	162.5	54.17	154.8			308.11						
165-170	167.5	55,83	CONT. IN 1922 TA MATERIAL TON OWN	THE RESERVE AND THE RESERVE AN		327.66				ļ		
170-175	172.5	57,50			115.9					į	+	4
175-180	177.5	59.17	175.6			368,54				ļ		
180-185	182.5		182.9				تية تعسم	32 ()			y	
180-185	182.5	60.83	182.9	312.9	130.0	389.87						1

Table 10: Operations Summary for Unit 52, 2011-2018

Unit 52 His	tory							
Generation	2018	2017	2016	2015	2014	2013	2012	201
MW	Hrs	Hrs	Hrs	Hrs	Hrs	Hrs	Hrs	Hrs
05	4012	3308	3365	4527	3767	5362	3647	3028
0-10	489	316	354	276	258	278	276	270
10-20	113	129	109	59	93	118	135	103
20-30	71	44	28	15	14	38	19	3
30-40	111	16	11	9	14	11	5	1
40-50	51	21	11	7	3	9	2	1
51-55	16	5	4	4	3	4	0	
56-60	12	11	7		6	0	3	
60-65	11	7	5	8	8	4		THE PARTY OF THE P
66-70	14	13	9	9	14	6	2	
71-75	27	9	17	10	15	5		1
76-80	46	26	30	63	12	14	12	2
81-85	152	43	67	68		11	16	5
86-90	267	99	394	245	219	22	16	10
91-95	634	667	657	318	283	61	124	13
96-100	460	545	571	322	325	167	158	13
101-105	411	658	669	313	429	223	340	18
106-110	406	531	516	267	348	207	290	18
111-115	369	524	495	260	412	258	433	19
116-120	331	429	366	280	342	265	382	23
121-125	310	404	339		356	261	448	27
126-130	198	335	221	240	307	261	398	28
131-135	120	221	198	203	337		465	39
136-140	70	167	136	197	280	222	401	. 34
141-145	33	110	92	175	279	261	A	51
146-150	14	64	49	110	159	138		35
151-155	11	37	36	82	179	136		65
156-160	0	20	15	65		48	118	21
161-165	. 0	0	12	189		30	51	20
166-170	0	0	0	173	Van Transfer & Francis and a	12	83	34
171-175	0	0	0	0		9	83	21
176-180	0	0	0	0			6	20
181-185	0	0	0	0	Ö	0	0	
186-200	0	0	0	0	0	0	0	
200-210	0	0	0	0		Õ	. 0	ar
210-220	0	0	0	0		0	, 0	
	8759	8759	8783	8759	8759	8759	8783	875

Table 11: Unit 52 Transformer Improvement

Mossyrock Xfmr BankLosses Value Calculation			Old Transformer	rests (per phase	e): U52		New Transfo	rmer Tests (per phase):	U52
			64.70	Rated Power (M	R/A)		77.00		
				No Load Loss				Rated Power (MVA)	
				Load Losses @		A ZIJAZILA		No Load Loss (kWh)	
			213.00	road résses @	rated MV	A (KVVII)	205.50	Load Losses @ Rated	MVA (kWh)
C	1	Each	Each (1 of 3)	Each (1 of 3)					
Generation MW		Xfmr Load	New Bank Loss		m.cc	Three			
05	Avg 0.25	0.08	New Bank Loss						
5-10	4.75					-3.899			
10-20	4.75					-3.639			
20-30	25					-1.301			
30-40	35					3.3197			
40-50	45					10.251			
						19.492			
51-55	53					28.548			
55-60	57.5					34.292			
60-65	62.5		63.2			41.223			
65-70	67.5		65.8			48.731			
70-75	72.5					56.817			
75-80	77.5			93.5	21.8	65.481			
80-85	82.5	27.50	74.9	99.8	24.9	74.722			
85-90	37 5	29.17	78.4	106.6	28.2	84.541			
90-95	92.5	30.83	82.0	113.7	31.6	94.937			
95-100	97.5	32.50	85.9	121.2	35.3	105.91			
100-105	102.5	34.17	89.9	129,1	39.2	117.46			
105-110	107.5	35.83	94.2	137.4	43.2	129.59			
110-115	112.5	37.50	98.7	146.1	47.4	142.3			
115-120	117.5	39.17	103.3	155.2	51.9	155.58			
120-125	122.5	40.83	108.2	164.7	56.5	169.44			
125-130	127.5	42.50	113.3	174.6	61.3	183.88			
130-135	132.5	44.17	118.6	184.9	66.3	198.9			
135-140	137.5	45.83	124.0	195.5	71.5	214.49			
140-145	142.5	47.50	129.7	206.6		230.67			
145-150	147.5	49.17	135.6	218.1	82.5	247.42			
150-155	152.5	50.83	141.7	230.0	88.2	264.74			
155-160	157.5		148.0	242.2		282.65			
160-165	162.5	54.17	154.5	254.9	100.4	301.13			
165-170	167.5	55.83	161.2	267.9		320,19			
170-175	172.5	57.50	168.1	281.4		339.83			
175-180	177.5	59.17	175.2	295.2		360.04			
180-185	182.5	60.83	182.5	309.4		380.84			
185-200	187.5	62.50	190.0	324.1		402.21			

FIGURE 19. Another Engineering Hydro RECS (MINYS) due to Transformer Replace medi-

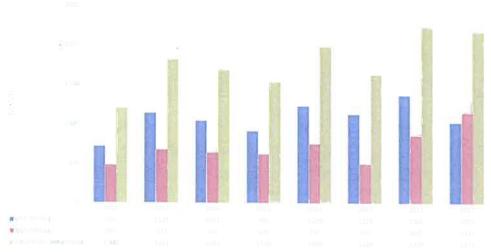


Figure 10 shows the annual incremental hydro results for years 2011-2018 for both Units 51 and 52. Beginning January 1, 2020, Tacoma Power plans to calculate actual annual incremental energy gain

(MWh) for the Mossyrock Transformer Replacement for Units 51 & 52 for Washington RPS Method One compliance using Equation 2 and the associated tables and figures described for future RPS compliance periods.

Engineering Review:

Mossyrock Rebuild Wicket Gate Calculations/Modeling

Mossyrock's Unit 51 and Unit 52 hydraulic turbines each have 20 identical wicket gates (or guide vanes) which control the flow of water through the turbines. The mechanism for the wicket gates forces them to move in unison, with matched angles and equal open areas. When opened, the area between the wicket gates forms a series of small openings around the turbine (see Figure 11). When closed, these gates form a relatively tight seal to minimize the leakage flow through the turbine so that the unit can be stopped; however, some leakage continues to squeeze past the wicket gates where they seal with each other (inter-gate leakage) and where they seal with the facing plates on the headcover and bottom ring (gate-end leakage).

Because Mossyrock's hydraulic turbines do not have upstream isolation valves, their wicket gates cannot be isolated after unit shutdown. Over the course of the year, the aforementioned leakage amounts to a significant amount of lost water (as high as 109 cfs before the rebuild, depending on lake elevation) and, thus, opportunity cost of lost generation.

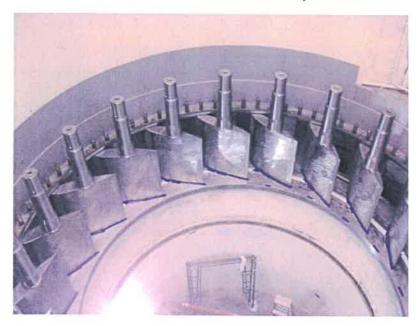


Figure 11: Photo of Wicket Gate Seal Replacement

During the turbine rebuilds in 2010 and 2011, the facing plates on the headcover and bottom ring were modified to accept bronze gate-end seals. These end seals minimized the gaps between the wicket gates and facing plates, thus reducing the gate-end leakage (to 5-13 cfs, depending on lake elevation) and storing additional water to be used for generation throughout the year (see Figures 11 and 12).



Figure 12: Lower Gate-End Seal with Wicket Gate in Open Position

Reduced wicket gate leakage (for Units 51 and 52) was calculated for "pre-" (before-) and "post-" (after-) upgrade leakage rates. The amount of saved water that can subsequently be used for generation is highly variable and depends on the amount of time the wicket gates are closed (i.e., the generator is turned off) and the elevation of Riffe Lake (see Tables 12 and 13). Steps to determine the wicket gate incremental savings are as follows:

- Determine Riffe Lake level ("Lake") and non-operating hours ("Hrs Not Operating") for Unit 51 & 52 from actual generation data.
- 2. Calculate the "Leak Rate" (cfs) at each lake level for the pre- and post-overhaul conditions using Equation 3, where Q_2 is the leak rate (cfs), z_{lake} is the lake level (ft), h_{ref} is the reference net head (ft) for the reference leak rate, and Q_{ref} is the reference leak rate (cfs) for the pre- or post-upgrade conditions.

$$Q2 = \sqrt{\frac{z_{lake} - 425 ft}{h_{ref}}} * (Qref)$$
 (Equation 3)

Reference leak rates (Q_{ref} values) of 109 cfs at 345 ft head were used for the pre-overhaul condition and 13.15 cfs at 345 ft net head for the post-overhaul condition. The 13.15 cfs value was based on the average of 3 tests completed on one unit in the 2009–2010 timeframe (see Table 12).

	20-May-09	10-Feb-10	10-Jun-10	
z_tail	425	425	425	
z_lake	765.7	719.75	770.45	
h_test	340.7	294.75	345.45	
Q_meas	12.91	10.90	14.68	
Adj to	351	351	351	energy part energy, can
Ratio	1.02	1.09	1.01	AVG
Qadj	13.1	11.9	14.8	13.27
Adj to	345	345	345	
Ratio	0 1.01 1.08 1.		1.00	AVG
Qadi	Qadj 12.99		14.67	13.15

Table 12: Mossyrock Leakage – Post-Rebuild Tests, 2009-2010

3. Calculate the estimated power loss ("Estimated PWR") (MW) associated with leakage in the preand post-upgrade conditions using Equation 4, where Q_2 is the leak rate (cfs), z_{lake} is the lake level (ft), and η_{TG} is the peak turbine-generator efficiency (94.58 %).

$$P = Q_2(z_{lake} - 430 ft) \left(0.0846 * 10^{-3} \frac{MW}{\left[\frac{S^2 * W * ft^4}{kg * m^2} \right]} \right) \eta_{TG} \quad \text{(Equation 4)}$$

- 4. Calculate the "Estimated Energy" (MWh) associated with leakage in the pre- and post-upgrade conditions by multiplying the power ("Estimated PWR") (MW) by the "Hrs. Not Operating" and summing all for each unit.
- 5. Subtract the post-upgrade "Estimated Energy" totals from the pre-upgrade "Estimated Energy" totals for each unit to find the annual energy savings associated with the wicket-gate refurbishment.

Mossy	rock Leakad	e Value				Referen	ce Points						T	1		T T	
				Unit		Leakage	Net Head	Time	ellne				-			1	
				L		cfs	ft		- 1					1		1	
				U51		109	345	Pre-Ov	rerhaul				1	1		-	
				US2	-	109	345	Pre-Ov			1				ilme ==		10 mm (d) 444 k
				U51		13,15	345	Post-O	verhaul				-	1 12	1555		
				U52		13.15	345		verhaul		0.00						
			1/2334				A 700										
		Un	lt 51			1	Unl	t 52			Unit	I Post Reno	vation	Unit	52 Post Reno	i	
	Hrs not	Leak rate	Estimate	Estim Energy		Hrs not			Estim Energy		Leak rate		E Lost Energy	Leak rate		E Lost Energy	
Lake	Operating	CFS	PWR (MW			Operating	CFS	PWR-MW	MW-Hr		CFS	Pwr-MW		CF5		MW-Hr	·
580		73.1			7= 7		73.1					1 101 -10100	14144-111	Cro	LAM -IMINA	- INIAA-HL	
						1				-	Passus		1				
665	0	90.9	1.71	0		0	90,9	1.71	0		11.0	0,21	0	11.0	0,21		
670	0	91.9	1.76	0		0	91,9	1.76	0		11.1	0.21	0	11.1	0.21	0	i
675	_0	92.8	1,82	0	1	0	92,8	1.82	0	. ,	11.2	0.22	0	11.2	0.21	0	
680	0	93,7	1.87	0		0	93,7	1,87	0	•	11.3	0.23	0	11.3	0.22	0	
605	0	94,6	1,93	0		0	94,6	1.93	0		11.4	0.23	0	11.4	0.23	0	
690	3	95,5	1,99	6		1	95.5	1.99	2 .		11.5	0.24	1	11.5	0.23	0	
695	598	96,4	2.04	1223		475	96.4	2.04	971		11.6	0.25	148		0.25	117	
700	55	97,3	2.10	116		32	97,3	2.10	67		11.7	0.25	14	11.6	-	4	
705	275	98.2	2.16	594		355	98.2	2.16	757		11.8	0.26	72	11.7	0.25	93	
710	781	99.1	2.22	1733		835	99.1	2.22	1853		12,0	0.27	209	11.8	0,26		·
715	214	99.9	2.28	488		276	99.9	2,28	629		12.1	0.27		12.0	0,27	224	
720	306	100.8	2.34	716		326	100.8	2,34	762		12.2	0.28	59 86	12.1	0.27	. 76	
725	650	101.6	2,40	1559		373	101,6	2,40	895		12.3	0.28	188	12,2	0,28	92	
730	408	102.5	2.46	1004		347	102.5	2,46	854		12.4			12.3	0.29	108	
735	382	103,3	2.52	963		339	103.3	2.52	855		12.5	0.30	121	12.4	0.30	103	
740	741	104.2	2,58	1914		698	104.2	2.58	1803					12.5	0.30	103	
745	344	105.0	2.65	910		391	105,0	2,65	1035	_	12.6	0.31	231	12.6	0.31	218	
750	0	105.8	2.71	0		0	105.8	2,71	0	-	12.7	0.32	110	12.7	0.32	125	
755	0	106.6	2.77	0		0	106.6	2,77			12.8	0,33	0	12,8	0.33	0	
760	0	107,4	2,84	0		0	107,4	2,84	0		12.9	0.33	0	12.9	0.33	0	*** *
765	0	108,2	2.90								13.0	0.34	0	13,0	0.34	0	
770	0	109.0	2.97	0		0	108.2	2,90	0		13.1	0.35	0	13.1	0.35	0	
775	0	109.8	3.03	0		0	109.0	2.97	0		13.2	0.36	0	13.2	0.36	0	
780	0	110.6	3.10	0	- 1	0		3,03	0	~~~~	13.2	0.37	0	13.2	0.37	0	V
otal	4757	110.0	3,10	11228	-	4448	110.6	3.10	0		13.3	0.37	0	13.3	0.37	0	
real	4/3/			11220	-	4448			10493				1355			1266	
	Estimated L	aakana Cra	dif for 1-937	1	-						-				ļ		
	The state of the	omando Ora	Cart 101 1-001	Energy Saving							i			- 4	ļ		
-	U51		who 100 mm - 110	9,872												i j	
	U52			9,227							1	in V					
	Total Leakag	a Savinac		19,099 N				- 11-			to the second			entire tak		i i	
	TOTAL LEAKAR	c addings		-(1a'0aa b	AIAAM .										. 191	1	

Table 13: 2018 Incremental Hydro Generation due to Wicket Gate Seal Replacement

This increase in generation will be recalculated each compliance year. Mossyrock's lake levels and hourly generation data are provided annually by Tacoma Power's Production Engineering group. Beginning January 1, 2020, Tacoma Power plans to calculate actual annual incremental energy gain (MWh) for the Mossyrock Wicket Gate Sealing Replacement using Equations 3 and 4 and associated tables and figures for Units 51 and 52 for future RPS Method One compliance.

Summary

Based on updated calculations/modeling Tacoma Power proposes to report Incremental Hydro savings for the rebuild of Units 51 and 52 at our Mossyrock project, including the turbine-generators, transformers, and wicket gate sealing systems completed in 2011, in accordance with WAC 194-37-130 (3) (c) (ii) Method One – actual incremental generation.

We are planning to amend our 2019 Renewable Compliance report originally submitted on May 31, 2019, to reflect revised calculations and modelling for the Mossyrock rebuild once actual 2019 Mossyrock generation data is available for the calculations (see Table 14). The 2019 Amendment will also re-calculate the appropriate Apprenticeship credit per WAC 194-37-136 (1) for the rebuild project.

Pending approval of this Advisory Opinion, we are targeting RPS 2019 Amendment by May 1, 2020 and 2020 RPS reporting by June 1, 2020.

Table 14: Estimated 2019 Mossyrock Rebuild Amendment based on 2018 Generation Data

Rebuild	2019	Est 2019			
Action	Reported	Amended			
	Generation	Generation			
	(MWh)	(MWh)			
Improved	86,255	24,534			
Turbine					
Efficiency					
Improved	270	1,200			
Transformer					
Efficiency					
Wicket Gate	12,500	19,099			
Sealing					
Totals	99,025	44,833			

Additional Vintage 2018/2019 eligible RECs currently owned by Tacoma Power will be reported/retired to cover the estimated 2019 RPS difference of 54,192 MWh for 2019 RPS compliance.



STATE OF WASHINGTON DEPARTMENT OF COMMERCE

1011 Plum Street SE • PO Box 42525 • Olympia, Washington 98504-2525 • (360) 725-4000 www.commerce.wa.gov

April 29, 2020

RE:

To: Michael Furze, Assistant Director, Energy Division

From: Glenn Blackmon, Manager, Energy Policy Office

Decision Memo – Advisory Opinions 2020-001 (Mossyrock Dam)

Digitally signed by: glenn.
blackmon@commerce.wa.gov

DN: CN = glenn

Clerkfood

blackmon@commerce.wa.gov Date: 2020.04.29 15:14:13 -07'00'

Recommendation

Issue advisory opinions concluding that the incremental generation due to efficiency improvements at the Mossyrock hydroelectric project owned by Tacoma Power, as calculated using the method submitted with the utility's application, qualifies as an eligible renewable resource for purposes of the Energy Independence Act, Chapter 19.285 RCW.

Background

The Energy Independence Act ("EIA," also known as I-937) requires that qualifying electric utilities use renewable resources to meet a specified portion of customers' energy requirements and establishes eligibility standards for renewable resources used to meet this requirement.

The EIA defines hydropower as a renewable resource, but it limits the eligibility of this resource to the incremental electricity produced as a result of efficiency improvements completed after March 31, 1999. The hydroelectric projects must be located in the Pacific Northwest, and the additional generation must not result in new water diversions or impoundments. Eligibility is also limited by ownership: The project must either be owned by a qualifying utility or owned by the federal government and marketed by the Bonneville Power Administration.

RCW 19.285.045 allows utilities and project owners to obtain an advisory opinion from Commerce regarding the eligibility of resources to meet a target under RCW 19.285.040. In this case, the advisory opinion from Commerce provides a basis to identify in the Western Renewable Energy Generation Information System the portion of each project's output that is eligible under the Washington renewable portfolio standard.

Procedural History

¹ RCW 19.285.030(12)(b).

Tacoma Power, a qualifying utility under the EIA, submitted an advisory opinion application for the Mossyrock project on Jan. 30, 2020, and completed payment of the advisory opinion fee on Feb. 20, 2020. The application included engineering analysis, stamped by a registered professional engineer, documenting data and methodology supporting Tacoma's request.

Commerce posted the application on its website and provided an opportunity for public comment, as required by RCW 19.285.045. It received no comments. Tacoma Power provided supplement information at the request of Commerce on April 7, 2020.

Analysis - Eligibility of the Incremental Generation

The engineering analysis describes the improvements made that resulted in increased generation. Tacoma Power completed comprehensive upgrades of the two units in the Mossyrock project in 2010 and 2011. The upgrades included generators and turbines, transformers, and wicket gates. As discussed below, the efficiency improvements meet each of the elements of the eligibility requirements in RCW 19.285.030(12)(b):

- The incremental generation must result from efficiency improvements. The turbine and generator replacements, transformer replacements, and wicket gate end seal replacements result in greater hydroelectric output for any given quantity of water passing directly through the turbines.
- The efficiency improvements must be completed after March 31, 1999. Tacoma Power's application and engineering analysis confirm that the utility completed the upgrades after the statutory date.
- A qualifying utility must own the hydroelectric generation project. Tacoma Power is a qualifying utility and owns the Mossyrock project.
- The hydroelectric generation projects must be located in the Pacific Northwest. The Mossyrock project is located on the Cowlitz River in Lewis County, Washington.
- The additional generation must not result in new water diversions or impoundments.
 Tacoma Power has made no changes to the amount of water available to or impounded by the project, so the additional generation did not result in new water diversions or impoundments.

Analysis - Amount of Incremental Generation

Tacoma Power has described in its engineering analysis the approach used to determine the amount of electricity generated with and without the efficiency upgrades. The analysis concludes that over the period from 2011 to 2018, the upgrades allowed the project to generate and average of 49,668 MWh per year of additional generation. The additional generation is 2.46% of total generation on average.

Tacoma Power will calculate incremental generation each year based on actual stream flows and using the models described in its engineering analysis. The actual generation amounts and percentages will vary from the averages described here.

Application 2020-001 Decision Memo – Advisory Opinions 2020-001 (Mossyrock) et. al. – Page 3

Conclusion

Incremental generation from the Mossyrock project is an eligible renewable resource under the Energy Independence Act, as long as the actual amount of incremental generation is determined each year using the method submitted with the utility's application.